

# Numerical modelling of dynamic compression tests on multi-layer Origami plates

J. Aranda-Ruiz<sup>1\*</sup>, M.M. Moure<sup>2</sup>

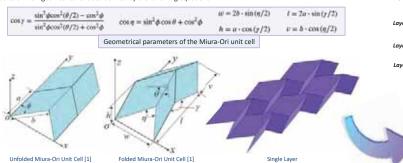
<sup>1</sup>Department of Continuum Mechanics and Structural Analysis <sup>2</sup>Department of Bioengineering and Aerospace Engineering \*jaranda@ing.uc3m.es



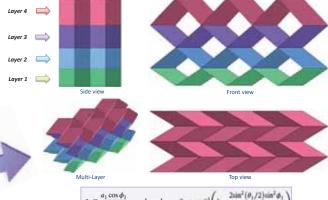
Abstract: In this work, the dynamic response of multi-layered Origami plates subjected to uniaxial compression tests has been numerically analyzed. The plates are based in the Miura-Ori single cell, which is defined through four independent geometrical parameters: two side lengths a and b, sector angle  $\phi$  and folding angle  $\theta$ . Four-layer specimens have been considered, and two different configurations: homogeneous or graded stiffness structures. Experimental results, involving quasi-static compression tests published in the scientific literature, have been used in order to validate the developed numerical model. The results show the influence of compression velocity: the slope of the densification area is higher as the compression velocity increases and the apparition of waves due to dynamic effects is more pronounced for higher velocities.

### 1. Description of the Problem

The problem analyzed consists on the uniaxial compression test of multi-layer Origami plates, in dynamic regime. The base geometry is the Miura-Ori unit cell, which can be defined using four independent geometrical parameters, which lead to six new geometrical entities defined by the following equations:



1.2. Geometry of the graded structure: To create a 3D structure with geometric gradient, layers with different sector angles are stacked in the out-of-plane z direction. In this case, the geometrical parameters must fulfil some additional constraints



## 1.1. Configurations analyzed:

- o Homogeneous structure:  $\phi_1=48^\circ$   $\phi_2=48^\circ$   $\phi_3=48^\circ$   $\phi_4=48^\circ$
- o Graded structure:  $\phi_1=42^\circ$   $\phi_2=46^\circ$   $\phi_3=50^\circ$   $\phi_4=54^\circ$

# 2. Material and Numerical Model

#### 2.1. Material properties for Brass (CuZn40)

The material of the main structure has been considered has elastic-plastic with linear hardening equation.

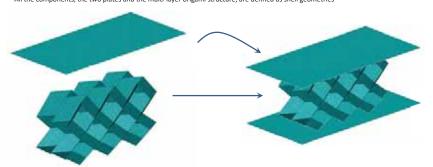
Density	$\rho$ = 8.33 g·cm <sup>-3</sup>
Elastic Modulus	E = 111.1 GPa
Poisson coeficient	$\nu$ = 0.346
Yield stress	$\sigma_y$ = 142 MPa
Tensile strength	$\sigma_u$ = 424.9 MPa
Flongation	$\varepsilon_u = 0.242$

#### 2.2. Material properties for steel: Material considered for the compressive plates

Density	$\rho$ = 7.85 g·cm <sup>-3</sup>
Elastic Modulus	E = 210.0 GPa

#### 2.3. Numerical model

All the components, the two plates and the multi-layer origami structure, are defined as shell geometries

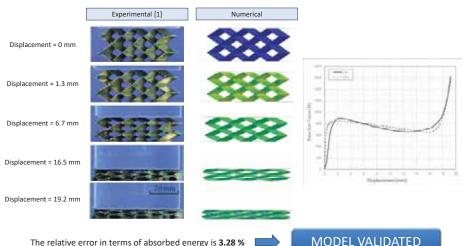


Model Information Number of 45600 S4R

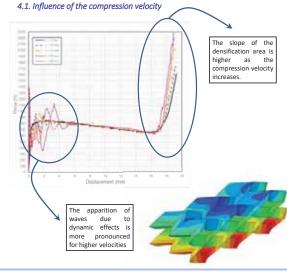
sin2d.

# 3. Validation

The numerical model has been validated with experimental results presented in the literature [1]



4. Results



# 5. Concluding Remarks

- O Using the Finite Element Method, a full 3-D numerical model of the compression tests in multi-layer metamaterial plate, has been implemented.
- O The numerical model has been validated with results published in the literature, leading to a relative error of about 3 %.
- O The morphological evolution of the structure during the compression process reproduce accurately the experimental
- O The apparition of waves in the initial stages of the compression test, due to dynamic effects, is more pronounced for
- O The value of the displacement at which the force stabilization occurs, increases with the compression velocity.
- O The slope of the densification area in the Force-Displacement curve is higher as the compression velocity increases
- O The model will be used in future investigations, analyzing different geometrical configurations.

The relative error in terms of absorbed energy is 3.28 %

# References

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[3] Mousanezhad D., Haghpanah B., Ghosh R., Hamouda A.S., Nayeb-Hashemi H., Vaziri A. Elastic properties of chiral, anti-chiral, and hierarchical honeycombs: a simple energy-based approach. Theoretical and Applied Mechanics Letters 2016; 6:81-96.

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